

(19) 世界知的所有権機関
国際事務局(43) 国際公開日
2004 年 10 月 21 日 (21.10.2004)

PCT

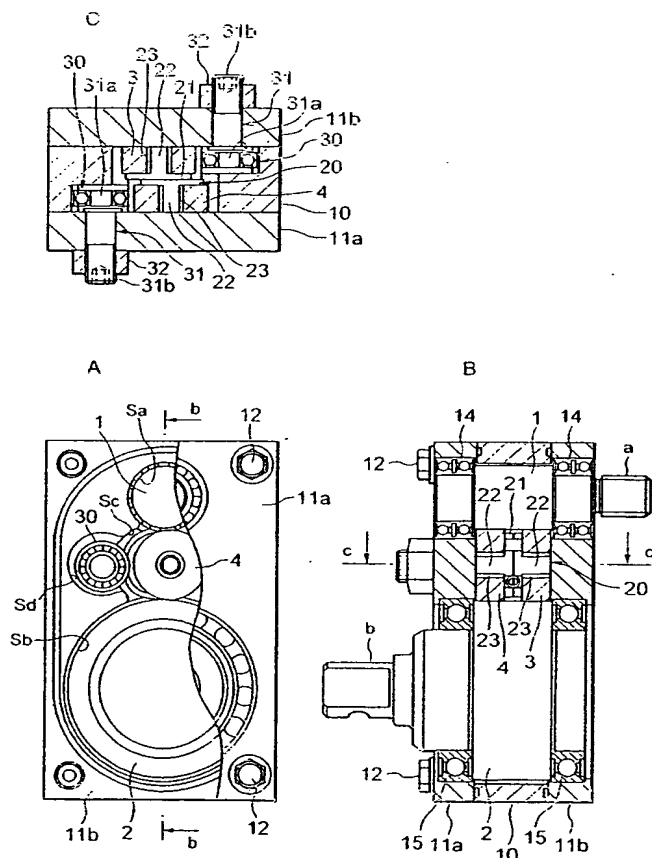
(10) 国際公開番号
WO 2004/090381 A1

- (51) 国際特許分類⁷: F16H 13/04
- (21) 国際出願番号: PCT/JP2004/005055
- (22) 国際出願日: 2004 年 4 月 8 日 (08.04.2004)
- (25) 国際出願の言語: 日本語
- (26) 国際公開の言語: 日本語
- (30) 優先権データ:
特願 2003-104284 2003 年 4 月 8 日 (08.04.2003) JP
- (71) 出願人 (米国を除く全ての指定国について): 日本精工株式会社 (NSK LTD.) [JP/JP]; 〒1418560 東京都品川区大崎 1 丁目 6 番 3 号 Tokyo (JP). NSK ステアリン
- (72) 発明者; および
- (75) 発明者/出願人 (米国についてののみ): 前田 篤志 (MAEDA, Atsushi) [JP/JP]; 〒3718528 群馬県前橋市総社町 1 丁目 8 番 1 号 NSK ステアリングシステムズ株式会社内 Gunma (JP). 力石 一穂 (CHIKARAISHI, Kazuo) [JP/JP]; 〒3718528 群馬県前橋市総社町 1 丁目 8 番 1 号 NSK ステアリングシステムズ株式会社内 Gunma (JP).
- (74) 代理人: 井上 義雄 (INOUE, Yoshio); 〒1030027 東京都中央区日本橋 3 丁目 1 番 4 号画廊ビル 3 階 Tokyo (JP).

/続葉有/

(54) Title: FRICTION ROLLER TYPE SPEED CHANGE GEAR

(54) 発明の名称: 摩擦ローラ式変速機



(57) Abstract: A friction roller type speed change gear in which a first roller (1) and a second roller (2) centering about a first shaft (1a) and a second shaft (2a) extending in parallel while being spaced apart from each other are arranged on the first roller (1) and the second roller (2) such that they do not abut each other, a third roller (3) and a fourth roller (4) abutting against both the first roller (1) and the second roller (2) are arranged between the first roller (1) and the second roller (2) oppositely on a line connecting the centers thereof, and a backup bearing (30) for regulating displacement of the third roller (3) and the fourth roller (4) by abutting against the third roller (3) and the fourth roller (4) is provided. Two supporting plates (11a, 11b) arranged on the opposite sides of the first roller (1) and the second roller (2) in the axial direction are provided with a bearing (14) for rotatably supporting the first roller (1) and the second roller (2), respectively, and the interval between these two supporting plates (11a, 11b) is set at a predetermined dimension by a setting member (10).

/続葉有/



(81) 指定国(表示のない限り、全ての種類の国内保護が可能): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BW, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NA, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RU, SC, SD, SE, SG, SK, SL, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, YU, ZA, ZM, ZW.

SZ, TZ, UG, ZM, ZW), ユーラシア (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), ヨーロッパ (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IT, LU, MC, NL, PL, PT, RO, SE, SI, SK, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

添付公開書類:

— 国際調査報告書

(84) 指定国(表示のない限り、全ての種類の広域保護が可能): ARIPO (BW, GH, GM, KE, LS, MW, MZ, SD, SL,

2文字コード及び他の略語については、定期発行される各PCTガゼットの巻頭に掲載されている「コードと略語のガイダンスノート」を参照。

(57) 要約:

互いに平行に離間した第1軸(1a)及び第2軸(2a)に、それぞれ第1軸(1a)及び第2軸(2a)を中心とする第1ローラ(1)と第2ローラ(2)とを互いに当接しないように配置し、第1ローラ(1)及び第2ローラ(2)の両方に当接するような第3ローラ(3)と第4ローラ(4)を、第1ローラ(1)と第2ローラ(2)の間かつ前記第1ローラ(1)と前記第2ローラ(2)の中心を結ぶ線に対峙するように配置し、かつ第3ローラ(3)及び第4ローラ(4)に当接して、第3ローラ(3)及び第4ローラ(4)の変位量を規制するバックアップ用軸受(30)をそれぞれ設けた摩擦ローラ式変速機において、第1ローラ(1)と第2ローラ(2)との軸方向両側に配置された2枚の支持板(11a、11b)は、これら第1ローラ(1)及び第2のローラ(2)をそれぞれ回転自在に支持する軸受(14)を備え、これら2枚の支持板(11a、11b)の間隔が設定部材(10)により所定寸法に定められている。

5 / prts 1

NSK2675PCTUS

DESCRIPTION

FRICTION ROLLER TRANSMISSION

5

Technical Field

The present invention relates to a friction roller transmission for transmitting torque while changing speed by means of a friction roller.

10

Background Art

In Japanese Patent Application Laid-Open Nos. 2002-349653 and 2003-28251 filed and laid open prior to this patent application, there is disclosed a friction roller transmission characterized in that:

15

a first roller and a second roller are disposed on two parallel shafts that are separated from each other in such a way that the rollers are not in contact with each other, the shafts being at the center of the respective rollers;

20

a third roller and a fourth roller that are in contact with both the first and the second rollers are disposed between the first roller and the second roller and on opposite sides with respect to the line connecting the center of the first roller and the center of the second roller; and

25

the angle formed by the tangential line of the

first roller and the third roller and the tangential line of the second roller and the third roller and the angle formed by the tangential line of the first roller and the fourth roller and the tangential line of the second roller and the fourth roller are
5 designed to be smaller than or equal to twice the respective angles of friction that are determined from the coefficients of friction between the respective rollers.

10 With the above features, it is possible to constitute a transmission path from the first roller to the third roller and then to the second roller, and another transmission path from the first roller to the fourth roller and then to the second roller,
15 thereby allowing both the forward and backward rotations in a backlash-free frictional roller transmission. It is also possible to minimize an increase in the working torque by generating a roller pressing power in accordance with the transmitted
20 torque, whereby the efficiency can be improved, particularly in the low transmitted torque range. In addition, since the rollers for power transmission are respectively provided for the rotation directions in such a way as to be in contact to the rollers,
25 torque transmission can be made possible without delay and without generating a slapping sound even when the direction of rotation is reversed.

A more specific description will be made in the following under an assumption that the first roller is the input side roller.

When the first roller is rotated clockwise (in
5 the CW direction), since the tangential line of the third roller and the first roller and the tangential line of the third roller and the second roller form an angle smaller than or equal to twice the friction angle, each contact angle is not larger than the
10 friction angle. Accordingly, relative slippage of the third roller and the first roller does not occur at their contact portion. Thus, a rotational force of the counterclockwise direction (in the CCW direction) is transmitted to the third roller by this
15 tangential force in the direction in which the third roller is brought closer to the first roller.

At the contact portion between the third roller and the second roller also, since the tangential line of the third roller and the first roller and the
20 tangential line of the third roller and the second roller form an angle smaller than or equal to twice the friction angle, each contact angle is not larger than the friction angle. Accordingly, relative slippage of the third roller and the second roller
25 does not occur at their contact portion. Thus, a tangential force acts on the second roller from the third roller, so that the second roller receives a

rotational force in the CW rotation direction. As the reaction, the third roller receives a tangential force in the opposite direction. This tangential force is in such a direction that the third roller is brought closer to the second roller.

The tangential forces acting on the third roller is a force biasing the third roller toward the first and the second rollers, and therefore, a pressing force corresponding to the tangential force transmitted or the torque can be obtained. The operation of the fourth roller is the same as the operation of the third roller except for the direction of rotation, and the description thereof will be omitted.

An improvement of the technology disclosed in the aforementioned Japanese Patent Application Laid-Open No. 2003-28251 is disclosed in Japanese Patent Application Laid-Open No. 2003-247617 that was filed by the applicant of the present patent application on February 21, 2002, which was prior to the priority date of the present patent application (that is, April 8, 2003) and laid open on September 5, 2003, the inventorship of which is the same as the inventorship of the present patent application). In this improvement, a setting member for setting the distance between two support plates that couples bearings that rotatably support the first and the

second rollers at both ends of these rollers to a predetermined dimension. The setting member is a cylindrical spacer through which a bolt on which a backup rolling bearing is attached is inserted or a
5 cylindrical spacer through which a bolt that secures the two support plate is inserted.

The aforementioned backup rolling bearing is provided in contact with the third or fourth roller so as to restrict displacement of the third or the
10 fourth roller to a predetermined amount. The backup rolling bearing is adapted to restrict displacement of the third roller or the fourth roller to a predetermined amount to prevent getting-over of the third or fourth roller and to prevent transmission of
15 torques larger than a predetermined torque.

As per the above, the distance between the two support plates can be set to a predetermined dimension by the setting member in the form of the cylindrical spacer. However, the volume of the
20 interior space in the friction roller transmission is large, and traction grease is scattered upon rotation of the rollers. Thus, A large amount of traction grease will be consumed.

Traction oil that constitutes the base oil of
25 traction grease has a very high evaporability, and it evaporates to cause a saturated state in the interior space of the friction roller transmission. This has

been one of the causes of deterioration of traction grease.

Disclosure of the Invention

5 The present invention has been made in view of the above described circumstances, and has as an object to provide a friction roller transmission in which scattering of traction grease is prevented, the consumption amount and the evaporation amount of
10 traction grease is reduced, and thereby the life of traction grease can be prolonged.

 To achieve the above object, according to the present invention, there is provided a friction roller transmission comprising:

15 a first roller and a second roller disposed on two parallel shafts that are separated from each other in such a way that the rollers are not in contact with each other, the shafts being at the center of the first and the second rollers
20 respectively;

 a third roller and a fourth roller that are in contact with both the first and the second rollers disposed between said first roller and said second roller, the third roller and the fourth roller being
25 opposite to a line connecting the center of the first roller and the center of the second roller; and

 backup bearings that are in contact with said

third and said fourth rollers respectively to restrict displacement amount of said third roller and said fourth roller;

5 characterized by two support plates disposed on both axial sides of said first roller and said second roller and having bearings for rotatably supporting the first and the second rollers respectively; and

a setting member for setting the distance between said two support plates to a predetermined
10 dimension.

As per the above, the friction roller transmission according to the present invention is provided with a setting member that sets the distance between the two support plate to a predetermined
15 dimension, and the volume of the interior space of the friction roller transmission is designed to be small. Therefore, it is possible to prevent scattering of traction grease, to reduce the consumption amount and the evaporation amount of
20 traction grease, and to thereby prolong the life of traction grease.

Preferably, said setting member may be a plate-like spacer disposed between said two support plates.

25 Brief Description of the Drawings

Fig. 1A is a side view of a friction roller transmission that constitutes a basic structure

according to the present invention.

Fig. 1B is a schematic perspective view of the friction roller transmission shown in Fig. 1A.

5 Fig. 2A is a side view of the friction roller transmission that constitutes the basic structure according to the present invention, showing a transmission path from the first roller to the fourth roller and then to the second roller.

10 Fig. 2B is a side view of the same kind showing a transmission path from the first roller to the third roller and then to the second roller.

In Figs. 3A to 3C that show a friction roller transmission according to an embodiment of the present invention, Fig. 3A is a partly cut-away front
15 view, Fig. 3B is a cross sectional view taken along line b-b in Fig. 3A, and Fig. 3C is a cross sectional view taken along line c-c in Fig. 3B.

20 Fig. 4 is an exploded cross sectional view of the friction roller transmission shown in Figs. 3A to 3C.

Fig. 5 is an exploded perspective view of the friction roller transmission shown in Figs. 3A to 3C.

Embodiment of the Invention

25 In the following, a friction roller transmission according to a preferred embodiment of the present invention will be described with reference to the

drawings.

(Basic Structure)

Fig. 1A is a side view of a friction roller transmission that constitutes the basic structure according to the present invention. Fig. 1B is a schematic perspective view of the friction roller transmission shown in Fig. 1A. Fig. 2A is a side view of the friction roller transmission that constitutes the basic structure according to the present invention, illustrating a transmission path from the first roller to the fourth roller and then to the second roller. Fig. 2B is a side view of the same kind illustrating a transmission path from the first roller to the third roller and then to the second roller.

In this basic structure of the friction roller transmission as shown in Figs. 1A, 1B, 2A and 2B,

a first roller 1 and a second roller 2 are disposed on two parallel shafts that are separated from each other in such a way that the rollers are not in contact with each other, the shafts being at the center of the respective rollers;

a third roller 3 and a fourth roller 4 that are in contact with both the first roller 1 and the second roller 2 are disposed between said first roller 1 and said second roller 2 and on opposite sides with respect to the line connecting the center

of the first roller 1 and the center of the second roller 2; and

an angle formed by a tangential line of the first roller 1 and the third roller 3 and a tangential line of the second roller 2 and the third roller 3 and an angle formed by a tangential line of the first roller 1 and the fourth roller 4 and a tangential line of the second roller 2 and the fourth roller 4 are designed to be smaller than or equal to twice the respective angles of friction that are determined from the coefficients of friction between the respective rollers, the frictional portions thereof being located outside the rollers.

In other words, letting P1 to P4 be the centers of the respective rollers, the rollers are designed in such a way that the sum of the angle formed by the line P1P2 and the line P1P3 ($\alpha_1: \angle P2P1P3$) and the angle formed by the line P1P2 and the line P2P3 ($\alpha_2: \angle P1P2P3$) and the sum of the angle formed by the line P1P2 and the line P1P4 ($\alpha_3: \angle P2P1P4$) and the angle formed by the line P1P2 and the line P2P4 ($\alpha_4: \angle P1P2P4$) are smaller than or equal to twice the friction angle ($\theta = \tan^{-1}\mu$) as formulated below.

$$\alpha_1 + \alpha_2 \leq 2\theta$$

$$\alpha_3 + \alpha_4 \leq 2\theta$$

In cases where the above-described arrangement is adopted, since the friction angle is small, the

third roller 3 and the fourth roller 4 are necessarily disposed in a overlapping manner along the axial direction.

By adopting the above-described structure, a pressing force can be created in accordance with the transmitted torque. Therefore, it is not necessary to apply forces required for frictional transmission, namely forces for pressing the third and the fourth rollers 3 and 4 against the first and the second rollers 1 and 2 respectively. However, it is preferable that weak pressing forces be applied for retaining the initial contact state when the roller is not rotating. Although each roller is composed of one roller, it may be composed of a plurality of rollers.

In the following, the operation of the structure will be described under the assumption that the first roller 1 is the input side roller.

As shown in Figs. 1B and 2B, when the first roller 1 is rotated clockwise (in the CW direction), since the angle formed by the tangential line of the third roller 3 and the first roller 1 and the tangential line of the third roller 3 and the second roller 2 is smaller than or equal to twice the friction angle, the respective contact angles are smaller than or equal to the friction angle. Accordingly, relative slippage between the third

roller 3 and the first roller 1 does not occur at their contact portion, and the third roller 3 receives a tangential force from the first roller 1. This tangential force is in such a direction that the
5 third roller 3 is brought closer to the first roller 1, and the third roller 3 receives a counterclockwise force (in the CCW direction) by this tangential force.

In the contact portion between the third roller 3 and the second roller 2 also, since the tangential
10 line of the third roller 3 and the first roller 1 and the tangential line of the third roller 3 and the second roller 2 form an angle smaller than or equal to the friction angle, the respective contact angles are smaller than or equal to the friction angle.

15 Therefore, relative slippage between the third roller 3 and the second roller 2 does not occur at their contact portion. Accordingly, the second roller 2 receives a tangential force from the third roller 3 and receives a rotational force in the CW
20 direction. As a reaction thereto, a tangential force in the opposite acts on the third roller 3. This tangential force is in such a direction that the third roller 3 is brought closer to the second roller 2.

25 As per the above, the tangential forces acting on the third roller 3 are in such a direction that the third roller 3 is pressed against the first

roller 1 and the second roller 2. Accordingly, a pressing force is created in accordance with the transmitted tangential force or torque.

In this case, as shown in Fig. 2A, slippage does not occur in the contact portions of the fourth roller 4. Accordingly, the fourth roller 4 receives tangential forces from the first and the second rollers 1 and 2. However, the forces are in such a direction that the fourth roller 4 is brought away from the first and the second rollers 1 and 2, and the fourth roller 4 is only rotating while in contact with the first roller 1 and the second roller 2.

When the rotation of the first roller 1 is reversed and it rotates in the CCW direction as shown in Figs. 1B and 2A, the operation of the fourth roller 4 and the operation of the third roller 3 are switched to each other. In this case, since the fourth roller 4 has been already in contact with the first roller 1 and the second roller 2, the direction of power transmission can be changed smoothly when the direction of rotation is changed.

What is required to enable torque transmission is that each of the third and the fourth rollers 3 and 4 are in contact with the first and the second rollers 1 and 2. To retain the contact state, weak pressing forces for pressing the third and the fourth rollers 3 and 4 against the first and the second

rollers 1 and 2 may be applied.

As per the above, according to this basic structure, it is possible to constitute a transmission path from the first roller 1 to the third roller 3 and then to the second roller 2, and a transmission path from the first roller 1 to the fourth roller 4 and then to the second roller 2 to make forward and backward rotation possible in a backlash-free friction roller transmission (speed-reduction transmission). In addition, since a roller pressing force in accordance with the transmitted torque is created, it is possible to minimize an increase in the working torque. Particularly, it is possible to improve efficiency in the transmission torque range. Moreover, since the rollers that are always in contact are provided for transmitting power in respective rotational directions, torque transmission can be realized without delay and without generating a slapping sound even upon reversal of the rotation direction.

(Embodiment of the Present Invention)

Figs. 3A to 3C show a friction roller transmission (speed-reduction transmission) according to an embodiment of the present invention. Fig. 3A is a partly cut-away front view, Fig. 3B is a cross sectional view taken along line b-b in Fig. 3A, and

Fig. 3C is a cross sectional view taken along line c-c in Fig. 3B.

Fig. 4 is an exploded cross sectional view of the friction roller transmission (speed-reduction transmission) shown in Figs. 3A to 3C. Fig. 5 is an exploded perspective view of the friction roller transmission (speed-reduction transmission) shown in Figs. 3A to 3C.

This embodiment embodies the above-described basic structure, and the arrangement of the first to the fourth rollers 1 to 4, the contact angles and the friction angle are designed to be the same as those in the basic structure.

As shown in Fig. 3A to 3C and Fig. 5, a pair of support plates 11a, 11b are disposed on both sides of a plate-like spacer 10. A plurality of bolts 12 passing through one of the support plates 11a and the plate-like spacer 10 are screwed into screw holes on the other support plate 11b thereby assembling the plate-like spacer 10 and the two support plates 11a, 11b.

Between the plate-like spacer 10 and the pair of support plates 11a, 11b, a pair of ring-shaped sealing members 13, 13 are interposed. The plate-like spacer 10 is made of a light-weight material such as an aluminum alloy and may be formed by casting such as die casting.

The two support plates 11a and 11b have the same thickness and the same shape. The support plates 11a and 11b respectively have holes for supporting a pair of bearings 14, 14 that rotatably support the shaft
5 1a of the first roller 1 and holes for supporting a pair of bearings 15 and 15 that rotatably support the shaft 2a, 2a of the second roller 2. The support plates 11a, 11b are made of a material having a coefficient of linear expansion substantially the
10 same as that of the third and the fourth rollers 3, 4.

In this embodiment, the shaft 1a of the first roller 1 is integral with the input shaft a, and the shaft 2a of the second roller 2 is integral with the output shaft b. Thus, this embodiment constitutes a
15 speed-reduction transmission.

Surfaces of the support plates 11a, 11b are used as sliding surfaces for the third and the fourth rollers 3, 4. In the case of conventional integral type housings, the bottom face of an opening for
20 allowing insertion of the third and the fourth rollers 3, 4 serves as a sliding surface, and therefore, it is difficult to apply finish processing thereto. In contrast, in this embodiment, the two support plates 11a, 11b have a simple plate-like
25 shape. Accordingly, finish processing of the sliding surfaces can be easily carried out. Alternatively, the support plates 11a, 11b can be punched out using

a press molding process or the like to eliminate the finish processing itself. In addition, they may be the same parts that are opposed to each other, a cost reduction can be achieved.

5 The third and the fourth rollers 3, 4 are held by two holders 20, 20 with an offset. Each holder 20 is composed of a flange portion 21 having a nearly semicircular cross section and a shaft portion 22. The respective flange portions 21, 21 and the shaft
10 portions 22, 22 of the two holders 20, 20 are offset from each other by a predetermined distance. The third and the fourth rollers 3, 4 are rotatably supported on the shaft portions 22, 22 of the holders 20, 20 respectively by means of the bearings 23, 23.

15 Backup rollers 30, 30 that are in contact with the third and the fourth rollers 3, 4 respectively are provided to restrict displacement the third and the fourth rollers 3, 4 to a predetermined amount. Each backup roller 30 is, for example, a rolling
20 bearing with an outer ring serving as the contact surface.

 In this embodiment, displacement of the third and the fourth rollers 3, 4 is restricted to the predetermined amount by the backup rollers 30, 30 in
25 the form of the backup rolling bearings to avoid getting-over of the third and the fourth rollers 3, 4 and to prevent transmission of torques larger than a

predetermined torque.

As shown in Figs. 3A-3C and 5, the plate-like spacer 10 mentioned above is hollowed out to have a continuous space composed of a basically cylindrical space Sa for housing only the first roller 1, a basically cylindrical space Sb for housing only the second roller 2, a basically cylindrical space Sc for housing only the third and the fourth rollers 3, 4 and basically cylindrical spaces Sd for housing only the backup rolling bearings 30. The spaces Sd for housing the rolling bearings 30 are spaces having a bottom that open on opposite surfaces of the spacer 10 at symmetrical positions to back up the third and the fourth rollers 3, 4.

As per the above, in this embodiment, the plate-like spacer 10 is disposed between the pair of support plates 11a, 11b, so that the support plates 11a, 11b are fixed with a predetermined distance therebetween. By increasing the precision of the thickness of the plate-like spacer 10, it is possible to fix the distance between the pair of support plates 11a, 11b with a higher degree of accuracy.

In addition, since the aforementioned spaces Sa to Sd are formed continuously in the interior of the plate-like spacer 10, it is possible to reduce the volume of the interior space of the friction roller transmission as much as possible, and it is possible

to prevent traction grease from scattering, reduce the consumption amount and the evaporation amount of traction grease, and lengthen the life of traction grease.

5 In the inner rings of the respective backup rolling bearings 30, mounting bolts 31 are fitted and fixed. The mounting bolts 31 are secured to the pair of support plates 11a and 11b respectively. Each mounting bolt 31 has a head portion 31a to be fitted
10 into the inner ring of the corresponding backup rolling bearing 30 and a shaft portion 31b having male threads formed thereon that are coaxial with each other. When the mounting bolt is attached, the male threads of the shaft portion 31b are screwed
15 into a nut 32.

The present invention is not limited to the embodiment described in the foregoing, but various modifications may be made thereon.

As described in the foregoing, the friction
20 roller transmission according to the present invention is provided with a setting member that sets the distance between the two support plate to a predetermined dimension, and the volume of the interior space of the friction roller transmission is
25 designed to be small. Therefore, it is possible to prevent scattering of traction grease, to reduce the consumption amount and the evaporation amount of

traction grease, and to thereby prolong the life of traction grease.

What is claimed is:

1. A friction roller transmission comprising:
a first roller and a second roller disposed on
two parallel shafts that are separated from each
5 other in such a way that the rollers are not in
contact with each other, the shafts being at the
center of the first and the second rollers
respectively;

a third roller and a fourth roller that are in
10 contact with both the first and the second rollers
disposed between said first roller and said second
roller, the third roller and the fourth roller being
opposite to a line connecting the center of the first
roller and the center of the second roller;

15 backup bearings that are in contact with said
third and said fourth rollers respectively to
restrict displacement amount of said third roller and
said fourth roller;

two support plates disposed on both axial sides
20 of said first roller and said second roller and
having bearings for rotatably supporting the first
and the second rollers respectively; and

a setting member for setting the distance
between said two support plates to a predetermined
25 dimension.

2. A friction roller transmission according to

claim 1, wherein said setting member comprises a plate-like spacer disposed between said two support plates.

- 5 3. A friction roller transmission according to claim 1 or 2, wherein bores for housing said first to fourth rollers respectively are continuously formed in said setting member.

Abstract

A friction roller transmission includes a first roller and a second roller disposed on two parallel shafts that are separated from each other in such a way that the rollers are not in contact with each other, the shafts being at the center of the first and the second rollers respectively, a third roller and a fourth roller that are in contact with both the first and the second rollers disposed between said first roller and said second roller, the third roller and the fourth roller being opposite to a line connecting the center of the first roller and the center of the second roller, and backup bearings that are in contact with said third and said fourth rollers respectively to restrict displacement amount of said third roller and said fourth roller. Two support plates are disposed on both axial sides of said first roller and said second roller. The support plates have bearings for rotatably supporting the first and the second rollers respectively. The distance between the two support plates are set to a predetermined dimension by a setting member.

FIG. 1A

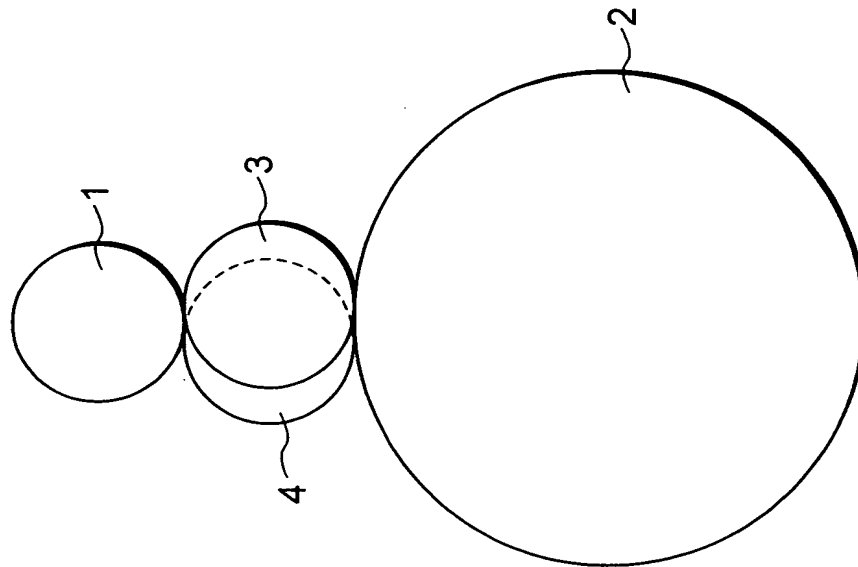


FIG. 1B

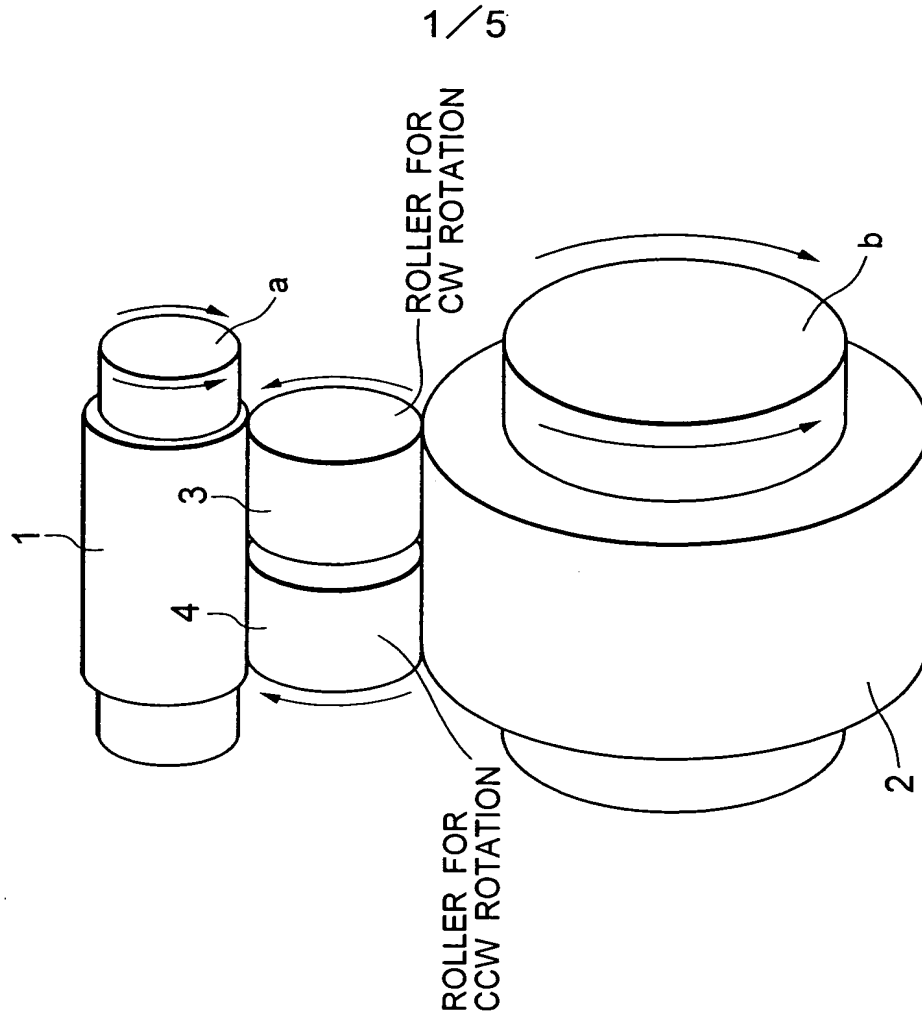


FIG. 2B

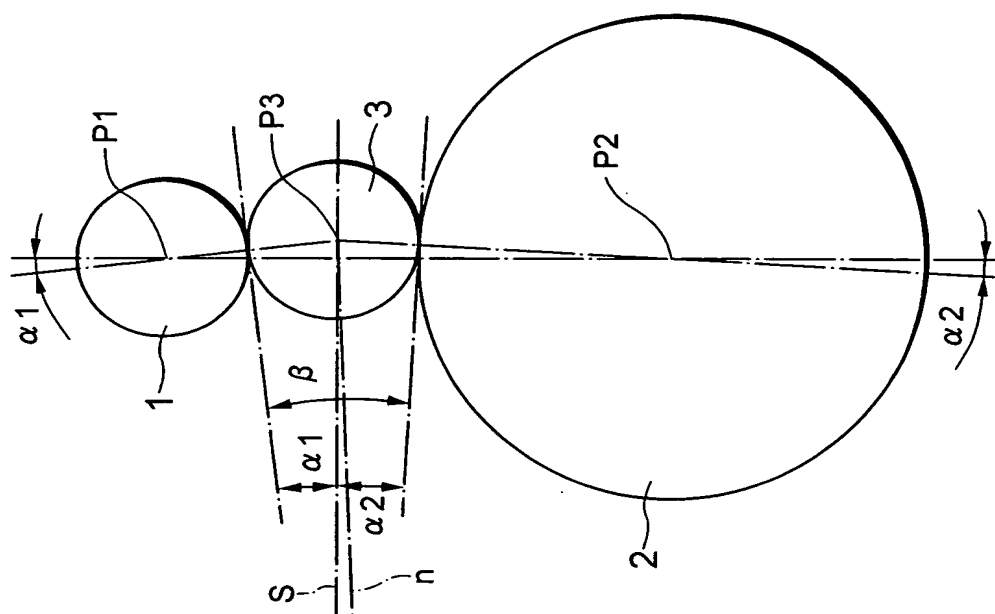


FIG. 2A

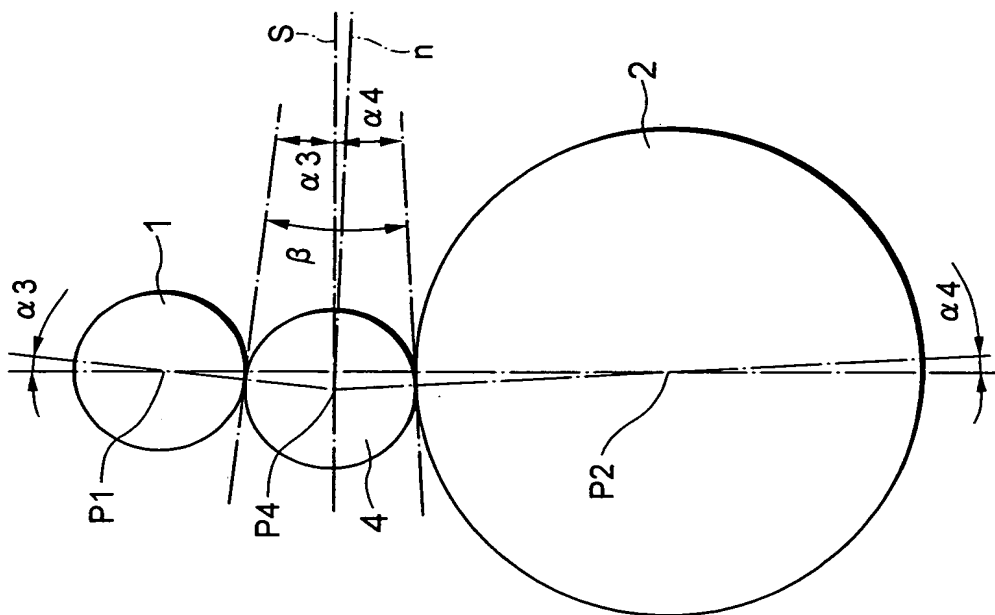


FIG. 3C

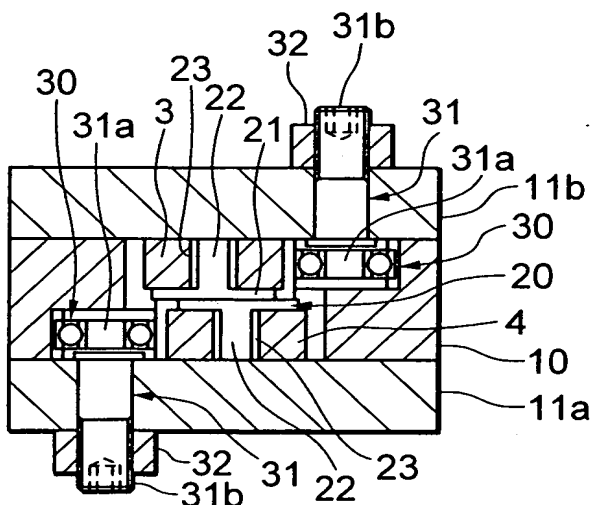


FIG. 3A

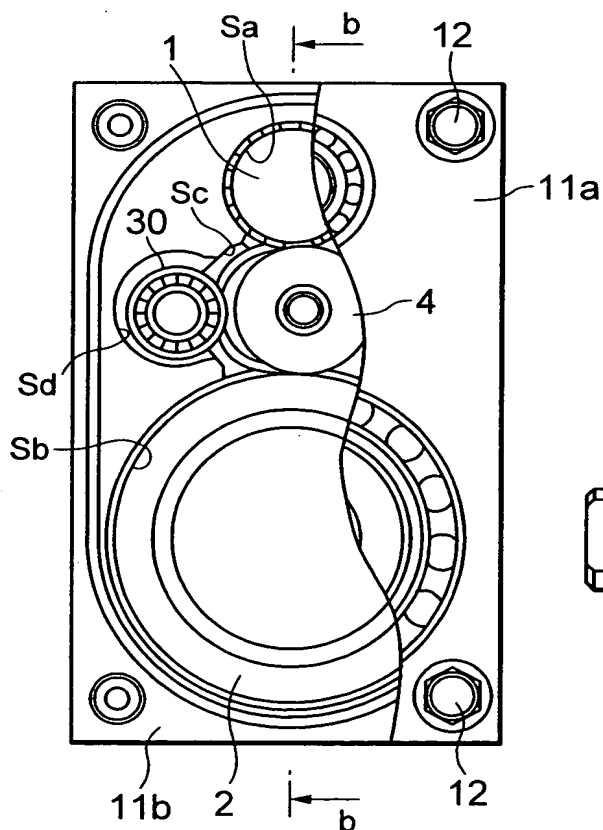


FIG. 3B

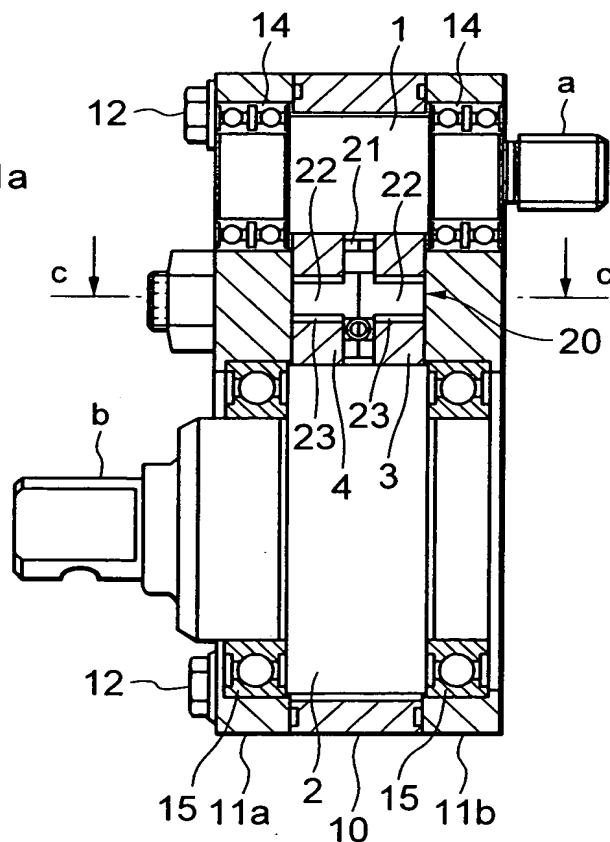


FIG. 5

